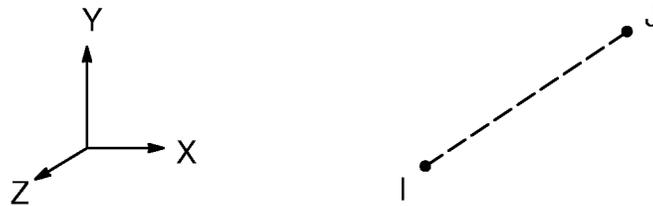


# 14.34 LINK34 — Convection Link



Matrix or Vector	Shape Functions	Integration Points
Conductivity Matrix	None used (nodes may be coincident)	None

## 14.34.1 Conductivity Matrix

The element conductivity (convection) matrix is

$$[K_c^t] = A h_f^{\text{eff}} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \quad (14.34-1)$$

where:

- $A$  = area over which element acts (input as AREA on **R** command)
- $h_f^{\text{eff}}$  = effective film coefficient, defined by equation (14.34-2)

The effective film coefficient is:

$$h_f^{\text{eff}} = \begin{cases} \text{maximum of } (h_f', C_c) & \text{if KEYOPT(3) = 3} \\ h_f' + C_c & \text{if KEYOPT(3) } \neq 3 \end{cases} \quad (14.34-2)$$

where:

- $h_f'$  = partial film coefficient term defined by equation (14.34-3)
- $C_c$  = input as CC on **R** command

The partial film coefficient term is:

$$h_f' = \begin{cases} F h_f & \text{if } n = 0.0 \\ F h_f |\Delta T_p|^n & \text{if } n \neq 0.0 \text{ and } \Delta T_p \neq 0 \\ 0.0 & \text{if } n \neq 0.0 \text{ and } \Delta T_p = 0 \end{cases} \quad (14.34-3)$$

where:

$$F = \begin{cases} T_B & \text{if } T_B > 0 \text{ and } \text{KEYOPT}(3) = 2 \\ 1.0 & \text{if } T_B \leq 0 \text{ or } \text{KEYOPT}(3) \neq 2 \end{cases}$$

$$T_B = \text{input quantity TBULK (input on **SFE** command)}$$

$$h_f = \begin{cases} & \text{if } \text{KEYOPT}(3) \neq 2 \\ H(m_e) & \text{or} \\ & \text{if } \text{KEYOPT}(3) = 2 \text{ and } h_f^{\text{in}} = 0.0 \\ H(-h_f^{\text{in}}) & \text{if } \text{KEYOPT}(3) = 2 \text{ and } h_f^{\text{in}} < 0.0 \\ h_f^{\text{in}} & \text{if } \text{KEYOPT}(3) = 2 \text{ and } h_f^{\text{in}} > 0.0 \end{cases}$$

$$H(x) = \text{input quantity CO on **MP, HF** command for material x}$$

$$m_e = \text{material number for this element (input on **MAT** command)}$$

$$h_f^{\text{in}} = \text{input quantity VAL1 (**SFE,,,CONV,1** command)}$$

$$\Delta T_p = T_{p,J} - T_{p,I}$$

$$T_{p,J} = \text{temperature from previous iteration at node J}$$

$$n = \text{input quantity EN on **R** command}$$

$\Delta T_p$  must be thought of as unitless, even though it is obviously derived from temperatures.

## 14.34.2 Output

The output is computed as:

$$Q = Ah_f^{\text{eff}} (T_I - T_J) \quad (14.34-4)$$

where:

$$Q = \text{output quantity HEAT RATE}$$

$$T_I = \text{temperature at node I}$$

$$T_J = \text{temperature at node J}$$